L8: Basic Concepts of Rigid-Body Dynamics

Hao Su

Spring, 2021

Some Further Clarifications on Velocity

- ullet Consider we observe the motion of a moving body b(t) from a moving observer's frame o(t), and the recording of motion is relative to s(t).
- velocity observed from an arbitrary frame (e.g., point linear velocity, angular velocity, and twist) is:

$$\left.m{v}_{s(t_0) o b(t_0)}^{o(t_0)} = \left.rac{\mathrm{d}}{\mathrm{d}t}p_{m{s(t)} o b(t)}^{o(t_0)}
ight|_{t=t_0}, \qquad ext{where } p_{s(t) o b(t)}^{o(t_0)} = p_{o(t_0) o b(t)}^{o(t_0)} - p_{o(t_0) o s(t)}^{o(t_0)}$$



Some Further Clarifications on Velocity

- Consider we observe the motion of a moving body b(t) from a moving observer's frame o(t), and the recording of motion is relative to s(t).
- velocity observed from an arbitrary frame (e.g., point linear velocity, angular velocity, and twist) is:

$$\left.m{v}_{s(t_0) o b(t_0)}^{o(t_0)} = \left.rac{\mathrm{d}}{\mathrm{d}t}p_{m{s(t)} o b(t)}^{o(t_0)}
ight|_{t=t_0}, \qquad ext{where } p_{s(t) o b(t)}^{o(t_0)} = p_{o(t_0) o b(t)}^{o(t_0)} - p_{o(t_0) o s(t)}^{o(t_0)}$$

- Note: above is a general rule of **taking derivative of coordinate w.r.t. time** (so that body velocity/twist is non-zero).
 - \circ e.g., when we derive the body-frame Euler equation last lecture, body inertia is defined by body frame coordinates, more precisely, $I_{b(t)}^{b(t_0)} = \int \mathrm{d}V \rho(r_{b(t) o x(t)}^{b(t_0)})[r_{b(t) o x(t)}^{b(t_0)}][r_{b(t) o x(t)}^{b(t_0)}]$
 - \circ Therefore, while I is an invariant w.r.t. t (since $r_{b(t) o x(t)}^{b(t_0)}\Big|_{t=t_0}$ is invariant), its derivative (taken only w.r.t. the subscript) is non-zero.
 - This is exactly the case that body-frame coordinate is a constant for body points, but they have velocity.

Agenda

- Kinetic Energy
- Change of Frame for Various Quantities
- Forward and Inverse Dynamics

click to jump to the section.



Kinetic Energy for Point Mass

• If a point mass m is moving with velocity $v_{s(t)\to b(t)}^o$ (s(t) is an inertia frame and the origin of b(t) is the point), then the kinetic energy of the point mass is

$$T_{s(t)
ightarrow b(t)} = rac{1}{2} m \|oldsymbol{v}^o_{s(t)
ightarrow b(t)}\|^2 \hspace{1cm} ext{(kinetic energy)}$$

Observer-Independence of Kinetic Energy

- Note that we omit observer's frame when describing kinetic energy, because it is independent of the observer's frame.
- ullet We prove by showing that $\|oldsymbol{v}_{s(t) o b(t)}^{o_1}\| = \|oldsymbol{v}_{s(t) o b(t)}^{o_2}\|$

Observer-Independence of Kinetic Energy

- Note that we omit observer's frame when describing kinetic energy, because it is independent of the observer's frame.
- ullet We prove by showing that $\|oldsymbol{v}_{s(t) o b(t)}^{o_1}\| = \|oldsymbol{v}_{s(t) o b(t)}^{o_2}\|$
- Proof:

6/25

$$egin{aligned} m{v}_{s(t) o b(t)}^{o_1} &= m{v}_{b(t)}^{o_1} - m{v}_{s(t)}^{o_1} = [m{\xi}_{b(t)}^{o_1} - m{\xi}_{s(t)}^{o_1}] p^{o_1} = T_{o_2 o o_1}^{-1} [m{\xi}_{b(t)}^{o_2} - m{\xi}_{s(t)}^{o_2}] T_{o_2 o o_1} p^{o_1} \ &= T_{o_2 o o_1}^{-1} [m{\xi}_{b(t)}^{o_2} - m{\xi}_{s(t)}^{o_2}] p^{o_2} = T_{o_2 o o_1}^{-1} (m{v}_{b(t)}^{o_2} - m{v}_{s(t)}^{o_2}) = T_{o_2 o o_1}^{-1} m{v}_{s(t) o b(t)}^{o_2} \ &= \begin{bmatrix} R_{o_1 o o_2} m{v}_{s(t) o b(t)}^{o_2} \|_{3 imes 1} \\ 0 \end{bmatrix} \begin{bmatrix} m{v}_{s(t) o b(t)}^{o_2} \|_{3 imes 1} \\ 0 \end{bmatrix} = \begin{bmatrix} R_{o_1 o o_2} m{v}_{s(t) o b(t)}^{o_2} \|_{3 imes 1} \\ 0 \end{bmatrix}$$

$$\|oldsymbol{v}_{s(t)
ightarrow b(t)}^{o_1}\| = \|oldsymbol{v}_{s(t)
ightarrow b(t)}^{o_2}\|$$



Observer-Independence of Kinetic Energy

- Note that we omit observer's frame when describing kinetic energy, because it is independent of the observer's frame.
- ullet We prove by showing that $\|oldsymbol{v}_{s(t) o b(t)}^{o_1}\| = \|oldsymbol{v}_{s(t) o b(t)}^{o_2}\|$
- Proof:

$$egin{aligned} m{v}_{s(t) o b(t)}^{o_1} &= m{v}_{b(t)}^{o_1} - m{v}_{s(t)}^{o_1} = [m{\xi}_{b(t)}^{o_1} - m{\xi}_{s(t)}^{o_1}] p^{o_1} = T_{o_2 o o_1}^{-1} [m{\xi}_{b(t)}^{o_2} - m{\xi}_{s(t)}^{o_2}] T_{o_2 o o_1} p^{o_1} \ &= T_{o_2 o o_1}^{-1} [m{\xi}_{b(t)}^{o_2} - m{\xi}_{s(t)}^{o_2}] p^{o_2} = T_{o_2 o o_1}^{-1} (m{v}_{b(t)}^{o_2} - m{v}_{s(t)}^{o_2}) = T_{o_2 o o_1}^{-1} m{v}_{s(t) o b(t)}^{o_2} \ &= \begin{bmatrix} R_{o_1 o o_2} m{v}_{s(t) o b(t)}^{o_2} |_{3 imes 1} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} m{v}_{s(t) o b(t)}^{o_2} |_{3 imes 1} \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} R_{o_1 o o_2} m{v}_{s(t) o b(t)}^{o_2} |_{3 imes 1} \\ 0 & 0 \end{bmatrix} \ &\therefore \|m{v}_{s(t) o b(t)}^{o_1}\| = \|m{v}_{s(t) o b(t)}^{o_2}\| \end{aligned}$$

We have also derived

$$m{v}_{s(t) o b(t)}^{o_1} = R_{o_1 o o_2}m{v}_{s(t) o b(t)}^{o_2} ext{ for } m{v} \in \mathbb{R}^3 \quad ext{(change of frame for velocities)}$$

- Integrate kinetic energy of every point mass over the body
- ullet We choose the body frame $\mathcal{F}_{b(t)}$ to start the derivation. Using the independence of observer's frame, we derive the formula to compute the energy in other frames.
- The origin of our body frame is always at the center of mass of the body



- Integrate kinetic energy of every point mass over the body
- We choose the body frame $\mathcal{F}_{b(t)}$ to start the derivation. Using the independence of observer's frame, we derive the formula to compute the energy in other frames.
- The origin of our body frame is always at the center of mass of the body
- The velocity of a body point $m{r}^{b(t)}$ is

$$egin{aligned} oldsymbol{v}_{s(t)
ightarrow b(t)}^{b(t)} &= [oldsymbol{\xi}_{s(t)
ightarrow b(t)}^{b(t)}] oldsymbol{r}^{b(t)} \ &= egin{bmatrix} [oldsymbol{\omega}_{s(t)
ightarrow b(t)}^{b(t)}] & oldsymbol{\dot{t}}_{s(t)
ightarrow b(t)}^{b(t)} \ 0 & 0 \end{bmatrix} oldsymbol{r}^{b(t)} \end{aligned}$$



Therefore,

$$egin{aligned} T_{s(t) o b(t)} &= \int_{m{r}^b \in B} rac{1}{2}
ho(x) \mathrm{d}V \|m{v}_{s(t) o b(t)}^{b(t)}\|^2 = \int_{m{r}^b \in B} rac{1}{2}
ho(x) \mathrm{d}V \|[m{\omega}_{s(t) o b(t)}^{b(t)}]m{r}^{b(t)} + m{t}_{s(t) o b(t)}^{b(t)}\|^2 \ &= (ext{some derivations using } [m{\omega}]m{r} = -[m{r}]m{\omega}) \ &= rac{1}{2} m \|m{t}_{s(t) o b(t)}^{b(t)}\|^2 + rac{1}{2} (m{\omega}_{s(t) o b(t)}^{b(t)})^T m{I}^b m{\omega}_{s(t) o b(t)}^{b(t)} \ &= rac{1}{2} (m{\xi}_{s(t) o b(t)}^{b(t)})^T m{m}^b m{\xi}_{s(t) o b(t)}^{b(t)} \end{aligned}$$

where

$$oldsymbol{\mathfrak{M}}^b = egin{bmatrix} m \mathrm{Id}_{3 imes 3} & 0 \ 0 & oldsymbol{I}^b \end{bmatrix} \in \mathbb{R}^{6 imes 6}$$



• Next, we introduce kinetic energy formula in other frames

- Next, we introduce kinetic energy formula in other frames
 - ullet Consider two frames \mathcal{F}_1 and \mathcal{F}_2 . Let $T_{1\to 2}$ be the change of coordinate transformation.
 - ullet To ensure that energy must be independent of the observer's frame, we **define** \mathfrak{M}^2 so that

$$rac{1}{2}(oldsymbol{\xi}^1)^T \mathfrak{M}^1 oldsymbol{\xi}^1 = rac{1}{2}(oldsymbol{\xi}^2)^T \mathfrak{M}^2 oldsymbol{\xi}^2$$



- Next, we introduce kinetic energy formula in other frames
 - ullet Consider two frames \mathcal{F}_1 and \mathcal{F}_2 . Let $T_{1 o 2}$ be the change of coordinate transformation.
 - ullet To ensure that energy must be independent of the observer's frame, we **define** \mathfrak{M}^2 so that

$$rac{1}{2}(oldsymbol{\xi}^1)^T \mathfrak{M}^1 oldsymbol{\xi}^1 = rac{1}{2}(oldsymbol{\xi}^2)^T \mathfrak{M}^2 oldsymbol{\xi}^2$$

ullet Recall that $oldsymbol{\xi}^1 = [\mathrm{Ad}_{1 o 2}] oldsymbol{\xi}^2$, and we conclude that

$$\mathfrak{M}^2 = [\mathrm{Ad}_{1 o 2}]^\mathrm{T} \mathfrak{M}^1 [\mathrm{Ad}_{1 o 2}]$$

(change of frame)

Change of Observer's Frame for Rotational Inertia Matrix

- ullet A side-product of introducing ${\mathfrak M}^o$ is that we can compute the inertia matrix in other frames conveniently
- We derived the change of frame formula for different body frames. What about frame change between general observer's frames?

Change of Observer's Frame for Rotational Inertia Matrix

- ullet A side-product of introducing \mathfrak{M}^o is that we can compute the inertia matrix in other frames conveniently
- We derived the change of frame formula for different body frames. What about frame change between general observer's frames?
- One can verify that,
 - the bottom-right 3×3 block of \mathfrak{M}^2 is the rotational inertial matrix in \mathcal{F}_2

Change of Frame for Various Quantities

Consider the right grasp problem

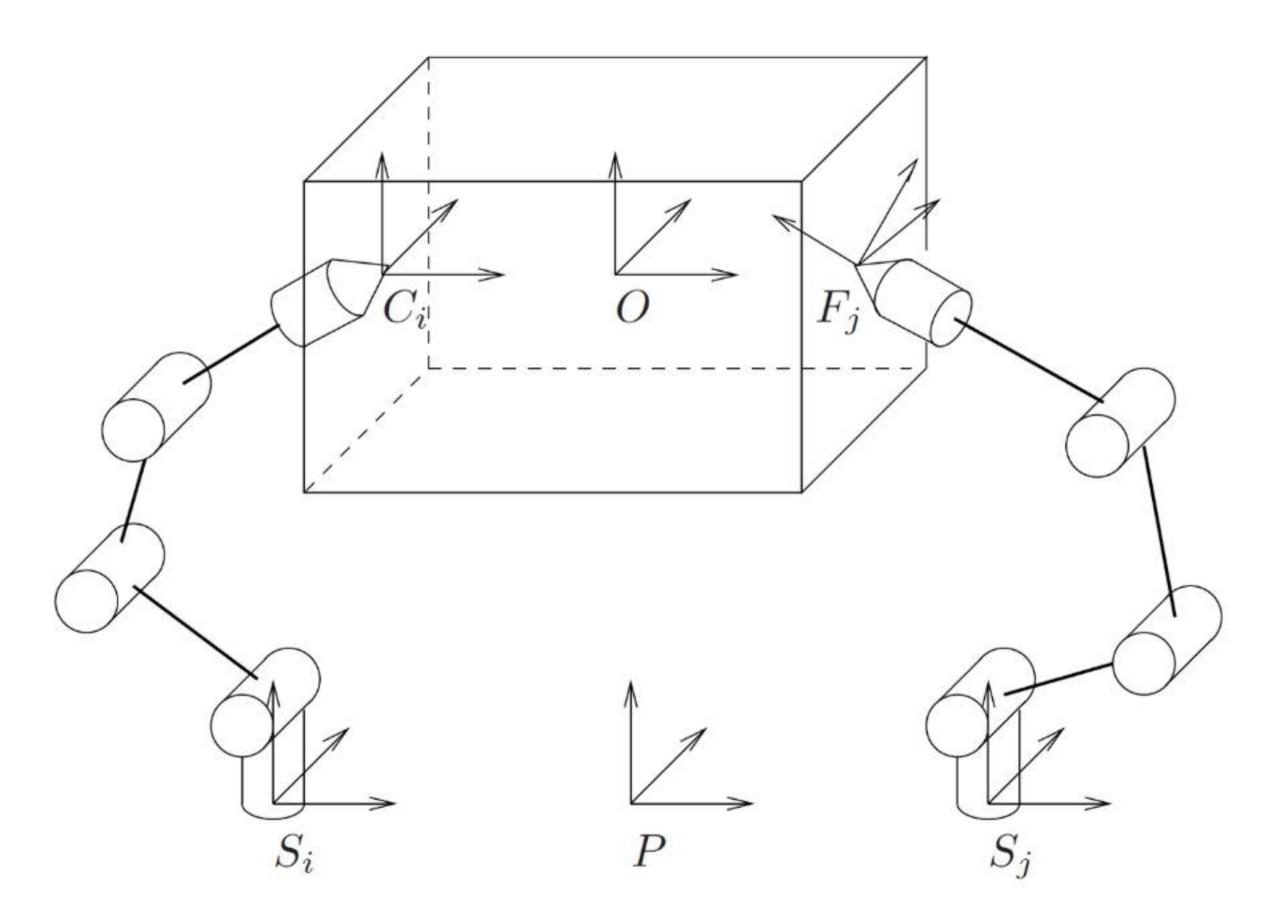


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms

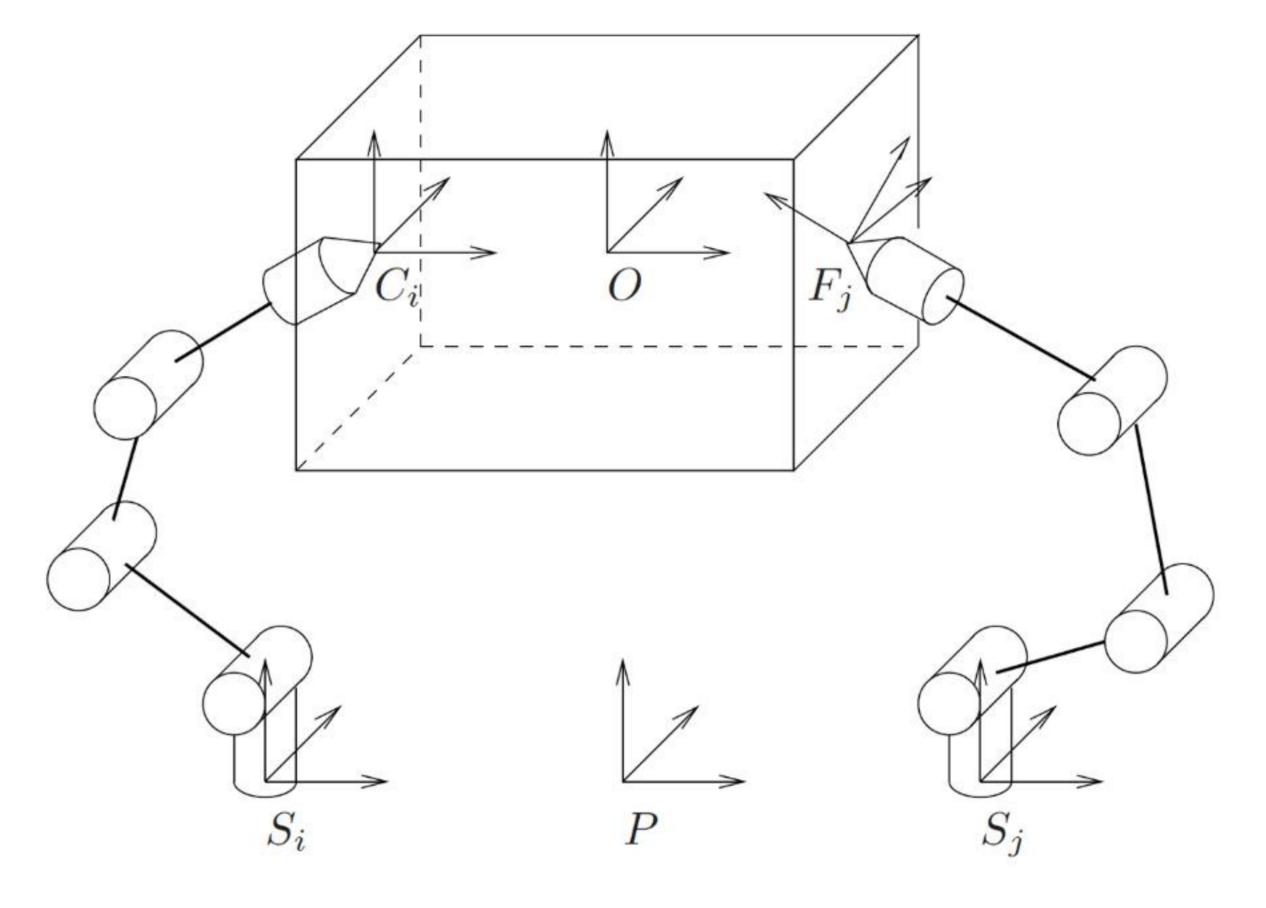


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors

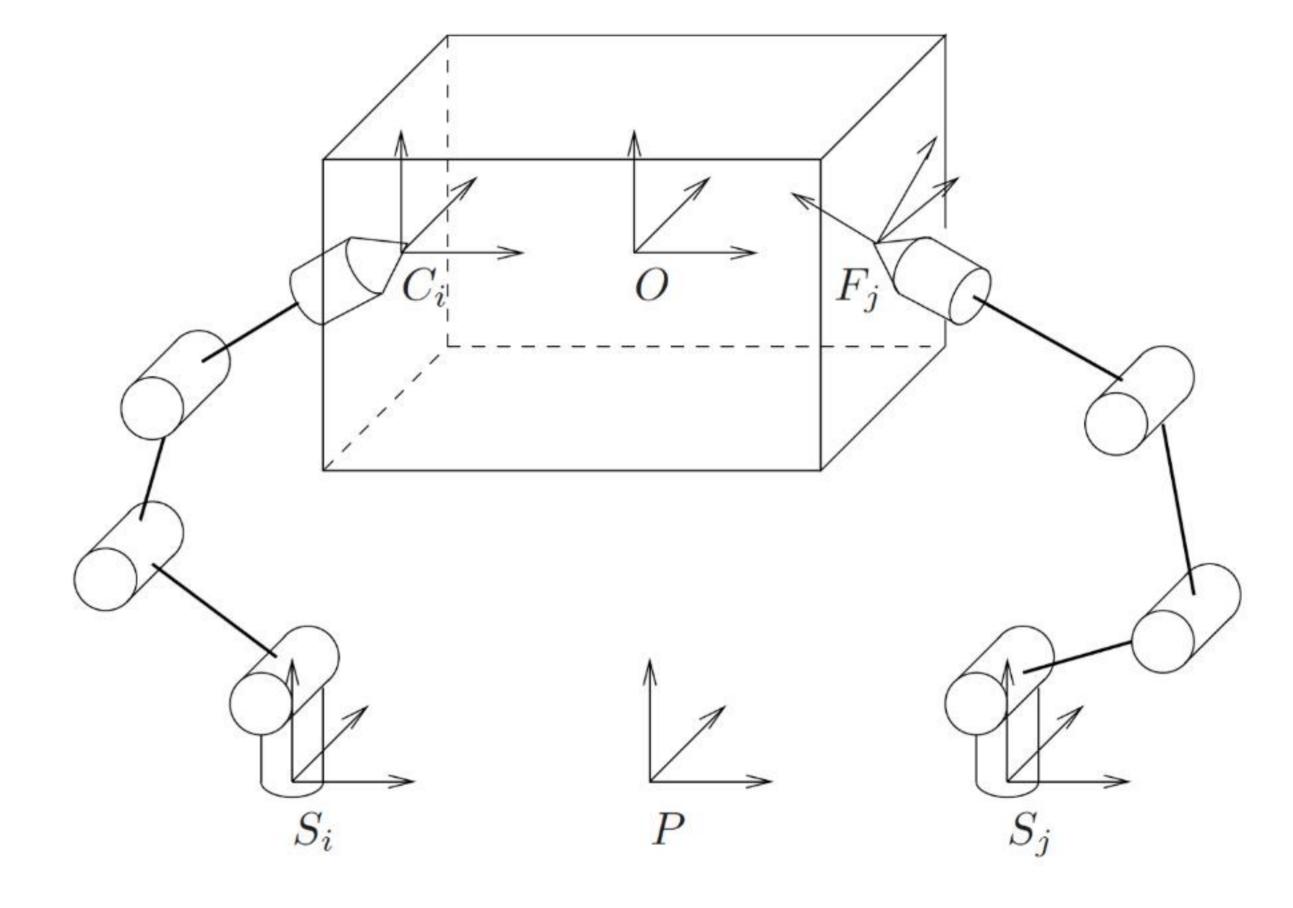


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors
 - These torques will be passed to the tips of the fingers.

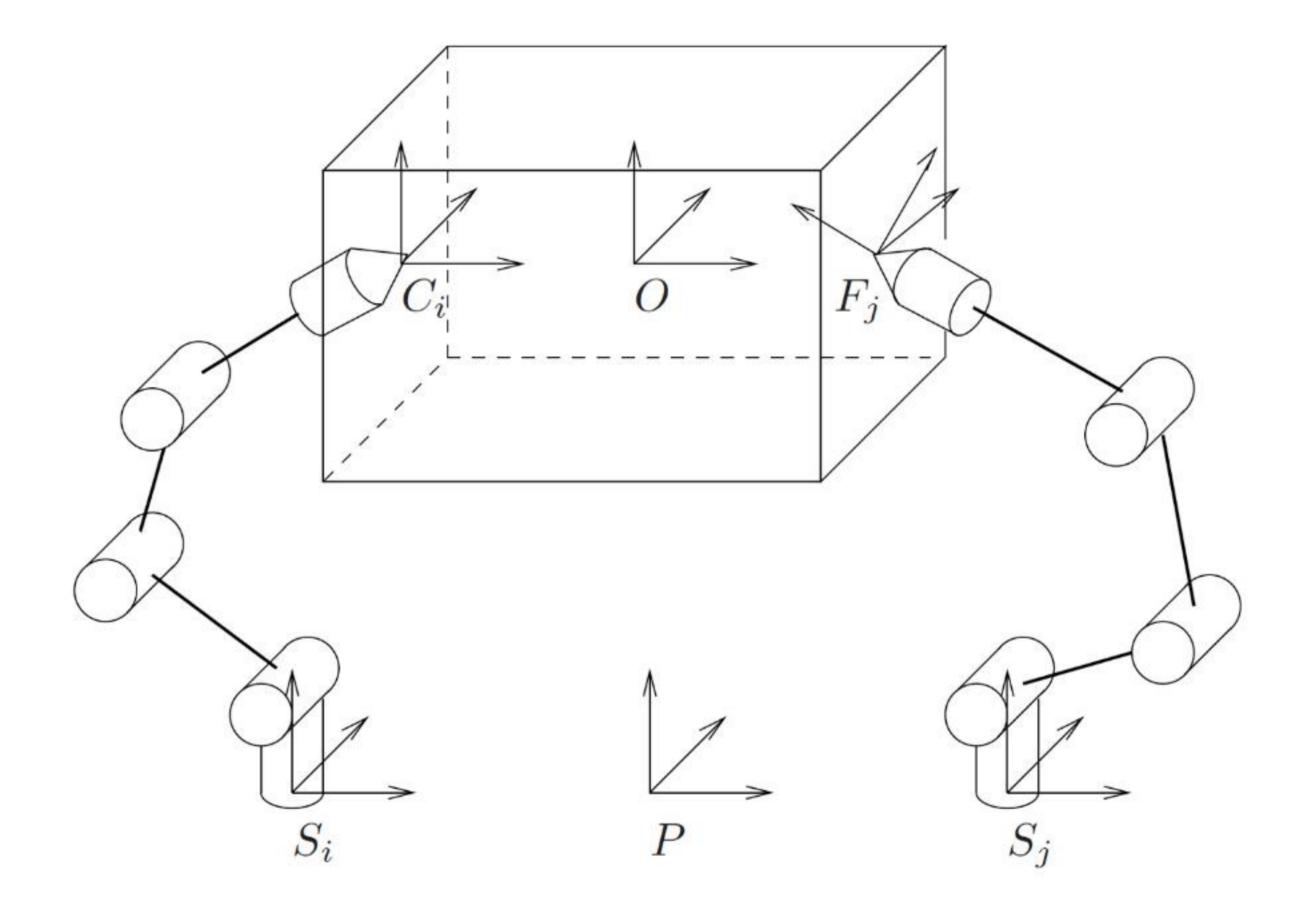


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors
 - These torques will be passed to the tips of the fingers.
 - The contact area will create certain force and torque at the contact point
 - force: pressure and friction
 - torque: e.g., anti-twisting friction force caused by the area contact

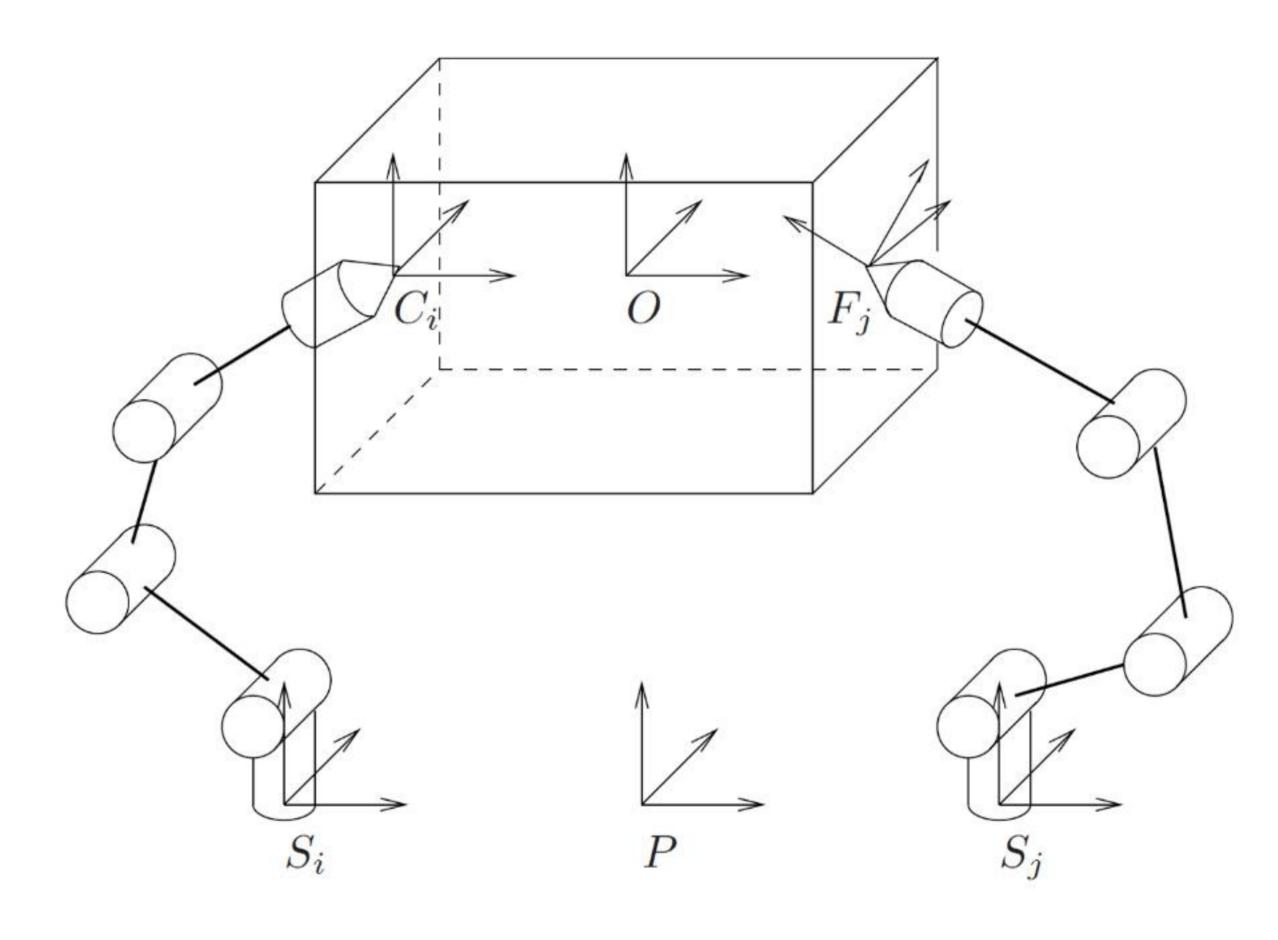


Figure 5.14: Grasp coordinate frames.

Contact Coordinate Frame

- ullet We build a **contact frame** C_i at each contact point
- The z-axis of the frame points inward along surface normal
- When recording force and torque at the contact point, it is natural to set C_i as the *observer's frame*, i.e.,

$$oldsymbol{F}^{C_i} = egin{bmatrix} oldsymbol{f}^{C_i} \ oldsymbol{ au}^{C_i} \end{bmatrix}$$

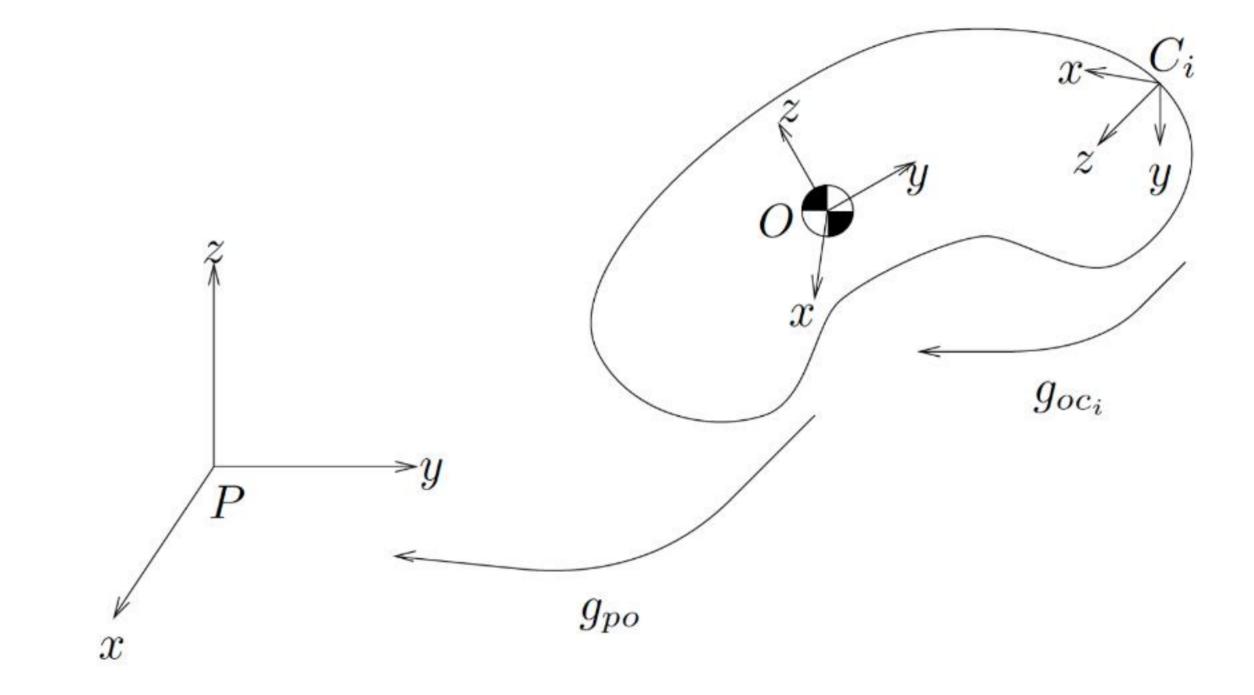


Figure 5.2: Coordinate frames for contact and object forces.

Some Kinds of Contact Forces

Contact Type	Frictionless point contact	Point contact with friction	Soft-finger
$oldsymbol{F}^C$	$egin{bmatrix} 0 \ 0 \ f_z \ 0 \ 0 \ 0 \ \end{bmatrix}$	$egin{bmatrix} f_x \ f_y \ f_z \ 0 \ 0 \ 0 \ \end{bmatrix}$	$egin{bmatrix} f_x \ f_y \ f_z \ 0 \ 0 \ au_z \end{bmatrix}$

Adding Forces and Torques

- Suppose we have calculated ${m F}^{C_i}$ at each contact (will learn later)
- What is the combined force and torque?

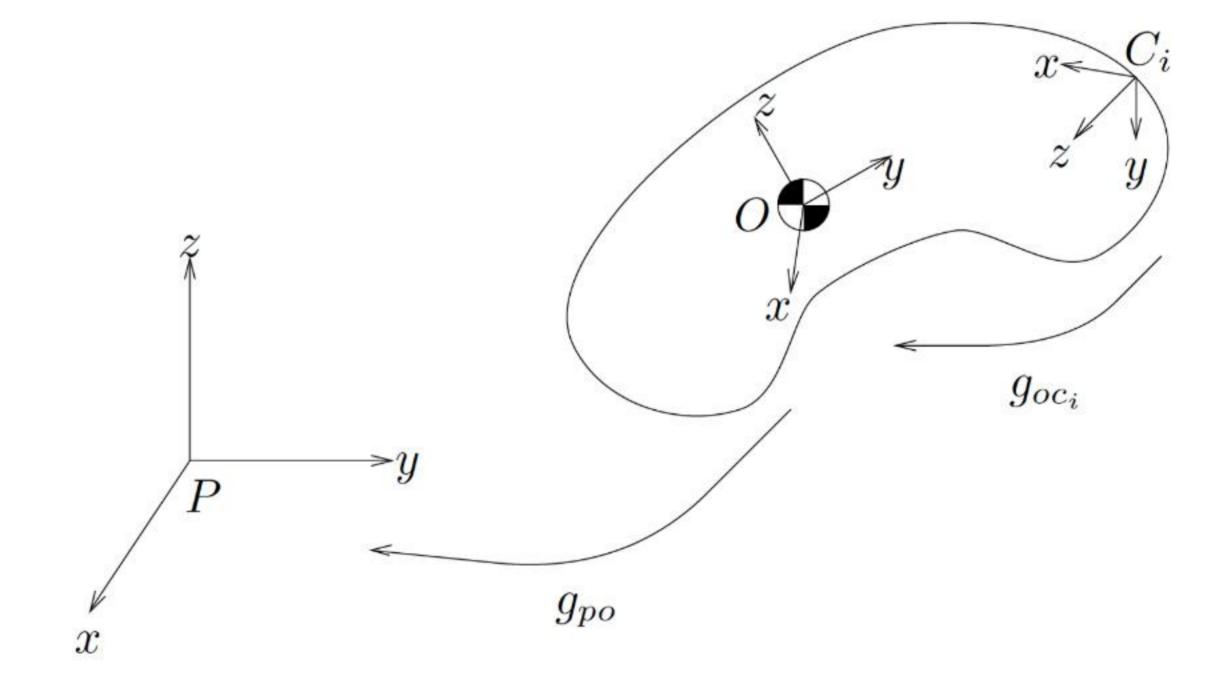


Figure 5.2: Coordinate frames for contact and object forces.

Adding Forces and Torques

- Suppose we have calculated ${m F}^{C_i}$ at each contact (will learn later)
- What is the combined force and torque?
- We cannot directly add forces and torques recorded using different observer frames

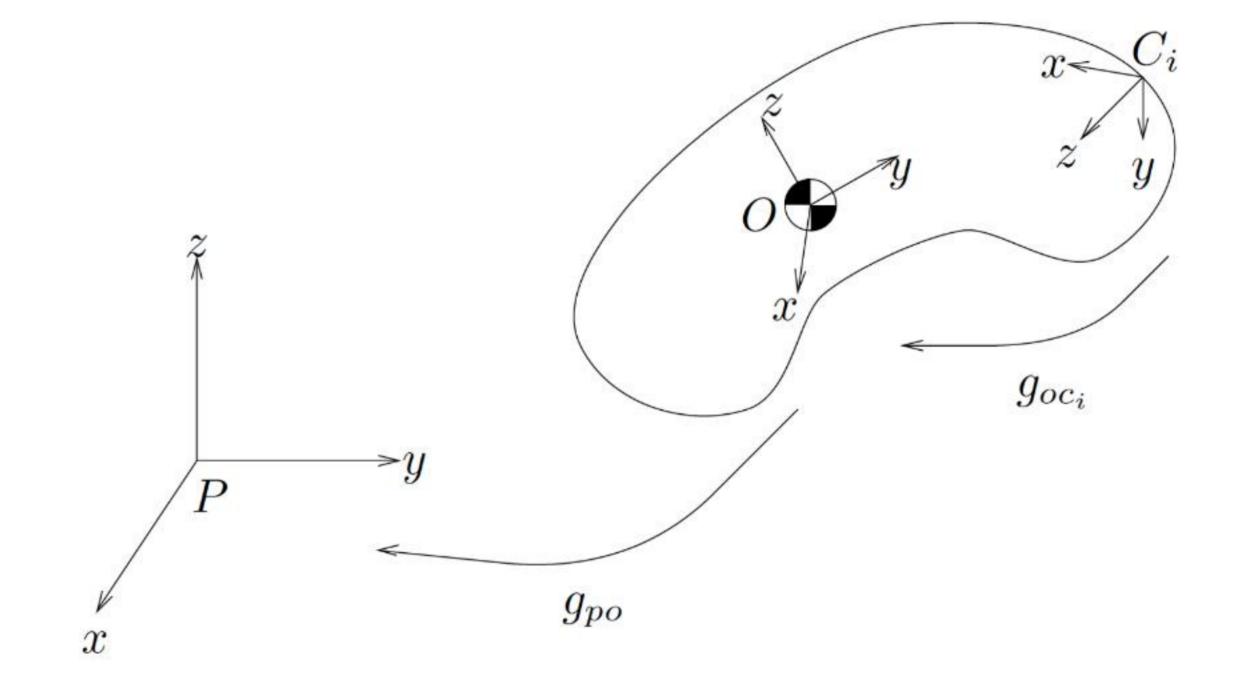


Figure 5.2: Coordinate frames for contact and object forces.

Adding Forces and Torques

- ullet Suppose we have calculated $oldsymbol{F}^{C_i}$ at each contact (will learn later)
- What is the combined force and torque?
- We cannot directly add forces and torques recorded using different observer frames
- However, we can change all to the same frame (e.g., body frame) and add together!

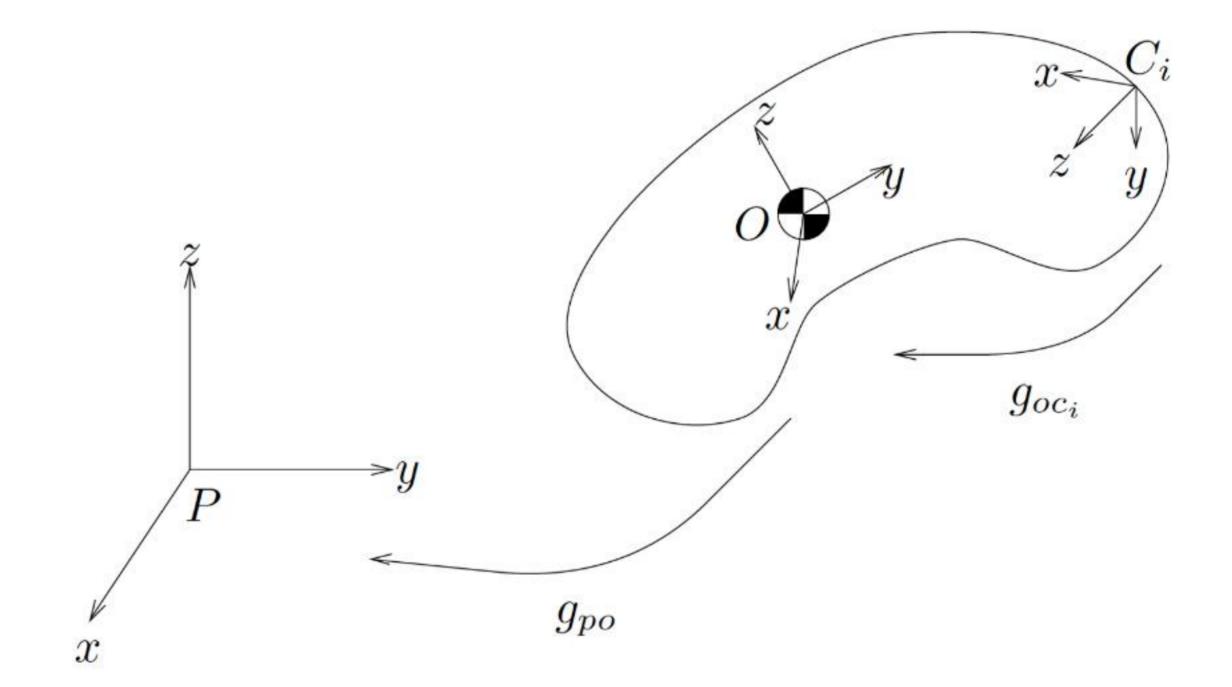


Figure 5.2: Coordinate frames for contact and object forces.

Change of Observer's Frame for Force and Torque

Consider the question of changing the observer's frame for force and torque

- We would relate
 - \circ $oldsymbol{f}^1$ and $oldsymbol{f}^2$
 - $m{ au}^1 = m{r}^1 imes m{f}^1$ and $m{ au}^2 = m{r}^2 imes m{f}^2$
- Note that

$$oldsymbol{r}^2 = R_{2 o 1}oldsymbol{r}^1 + oldsymbol{t}_{2 o 1}$$
 $oldsymbol{f}^2 = R_{2 o 1}oldsymbol{f}^1$

• Plug in the definition, and we derive that

$$egin{bmatrix} m{f}^2 \ m{ au}^2 \end{bmatrix} = egin{bmatrix} R_{2 o 1} & 0 \ [m{t}_{2 o 1}]R_{2 o 1} & R_{2 o 1} \end{bmatrix} egin{bmatrix} m{f}^1 \ m{ au}^1 \end{bmatrix} = (\mathrm{Ad}_{1 o 2})^\mathrm{T} egin{bmatrix} m{f}^1 \ m{ au}^1 \end{bmatrix}$$

Change of Observer's Frame for Force and Torque

• Define $m{F}^o = egin{bmatrix} m{f}^o \ m{ au}^o \end{bmatrix}$, then formula for change of frame is:

$$m{F}^2 = (\mathrm{Ad}_{1 o 2})^\mathrm{T} m{F}^1$$
 (change of frame)

• Using definitions and frame change equations, it is easy to verify that the following equation to compute the **power** of the system input (change rate of kinetic energy):

$$(oldsymbol{F}^b)^T oldsymbol{\xi}^b = (oldsymbol{F}^o)^T oldsymbol{\xi}^o = rac{\mathrm{d}T}{\mathrm{d}t}$$
 (system input power)

Solution to Adding Forces and Torques

$$m{F}^b = \sum_{i=1}^k [\mathrm{Ad}_{\mathrm{C_i}
ightarrow b}]^{\mathrm{T}} m{F}^{\mathrm{C_i}}$$

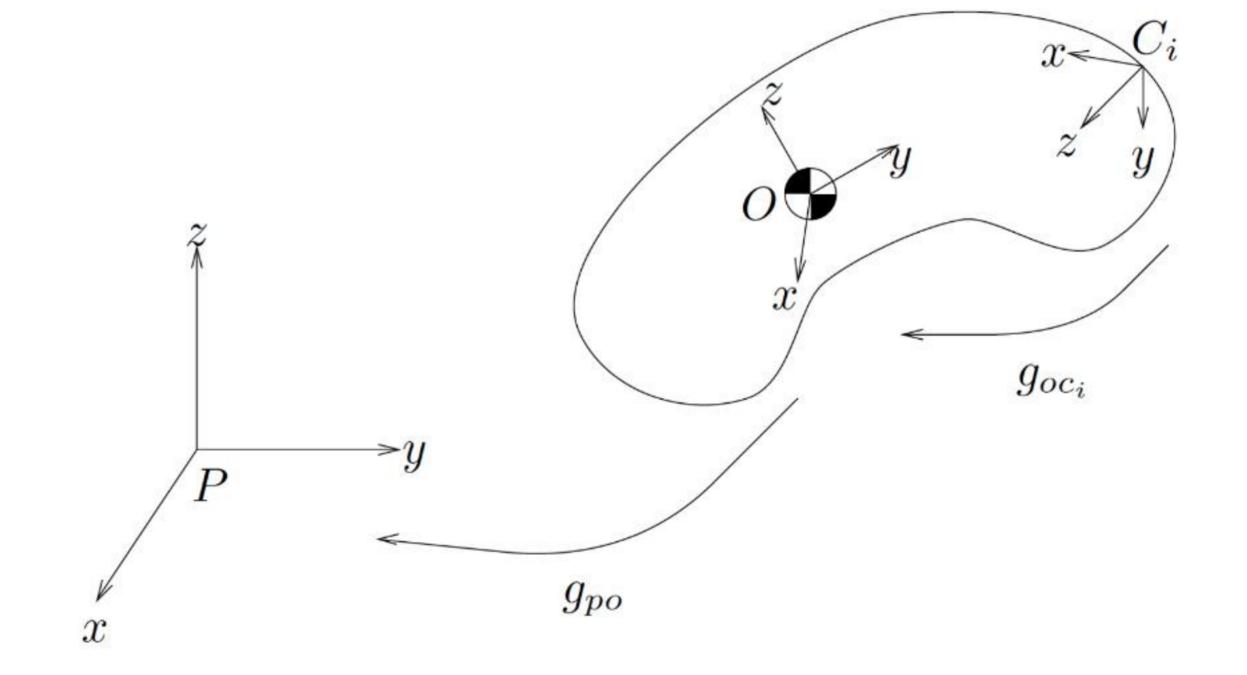


Figure 5.2: Coordinate frames for contact and object forces.

Change of Observer's Frame for Momentum and Angular Momentum

Consider the question of changing the observer's frame for momentum and angular momentum

- We would relate
 - $m{ ilde{p}}^1 = mm{v}^1$ and $m{p}^2 = mm{v}^2$
 - $m{\sigma} \; m{L}^1 = m{r}^1 imes mm{v}^1$ and $m{L}^2 = m{r}^2 imes mm{v}^2$
- Note that

$$egin{aligned} oldsymbol{r}^2 &= R_{2 o 1}oldsymbol{r}^1 + oldsymbol{t}_{2 o 1} \ oldsymbol{v}^2 &= R_{2 o 1}oldsymbol{v}^1 \end{aligned}$$

ullet The same derivation as force and torque pair, and we get $egin{bmatrix} m{p}^2 \ m{L}^2 \end{bmatrix} = (\mathrm{Ad}_{1 o 2})^\mathrm{T} egin{bmatrix} m{p}^1 \ m{L}^1 \end{bmatrix}$

Read by Yourself

Change of Observer's Frame for Momentum and Angular Momentum

• Define $m{P}^o = egin{bmatrix} m{p}^o \ m{L}^o \end{bmatrix}$, and the formula for change of frame is:

$$oldsymbol{P}^2 = (\mathrm{Ad}_{1 o 2})^\mathrm{T} oldsymbol{P}^1 \qquad \qquad ext{(change of frame)}$$

• Note: similar to linear momentum that $\mathbf{p}^o = \frac{\mathrm{d}T}{\mathrm{d}\mathbf{v}^o}$ for translation-only motion, it is straight-forward to verify that

$$m{P}^o = rac{dT}{dm{\xi}^o} = m{\mathfrak{M}}^o m{\xi}^o \hspace{1.5cm} ext{(generalized angular momentum)}$$

Summary

- We have learned basic concepts for body motion dynamics
 - Properties of objects: mass, rotational inertia
 - Motion state: momentum, angular momentum
 - Action: force, torque
 - Energy perspective: kinetic energy
- We have also introduced various equations for changing the observer's frame

Forward and Inverse Dynamics

Consider the right grasp problem

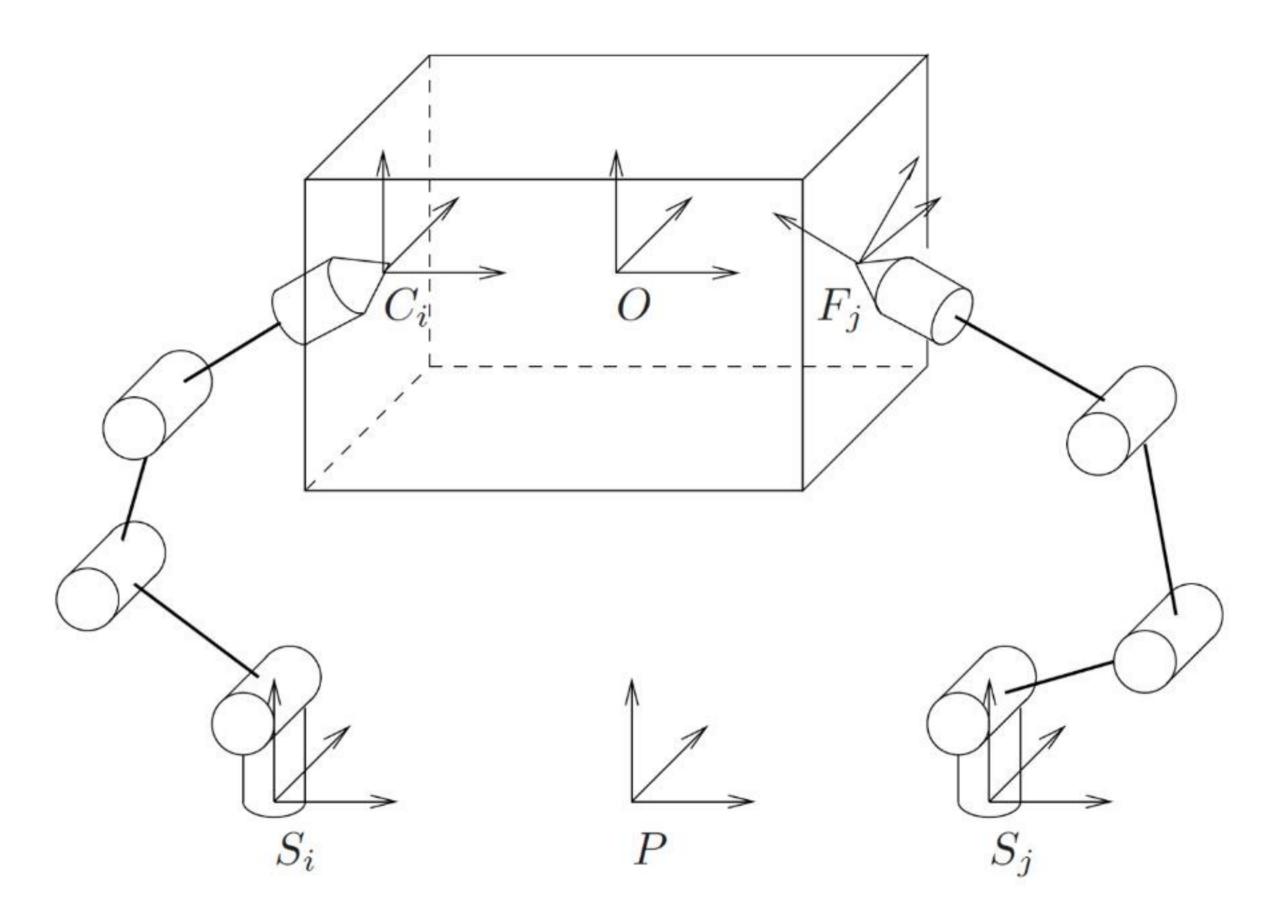


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms

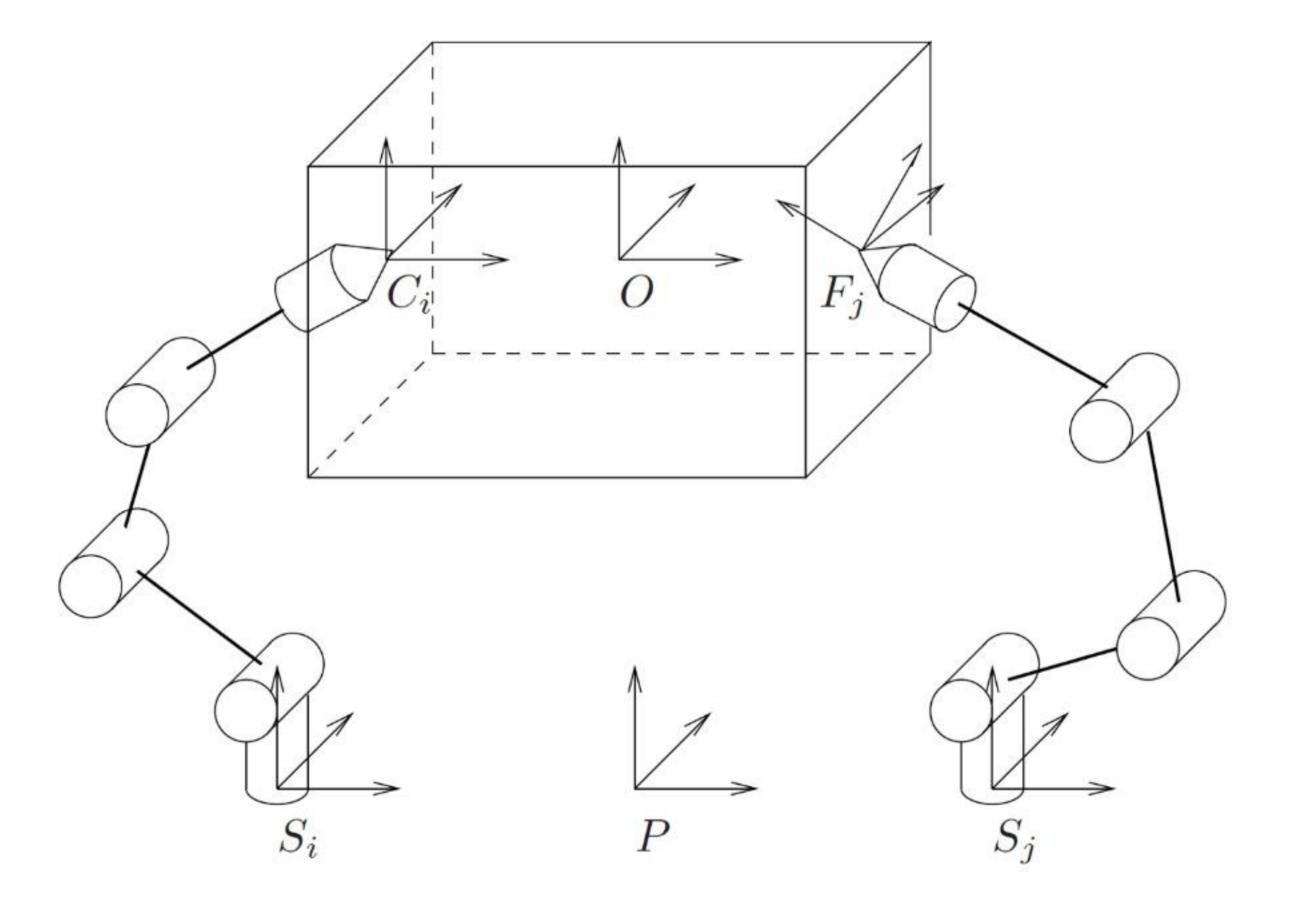


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors

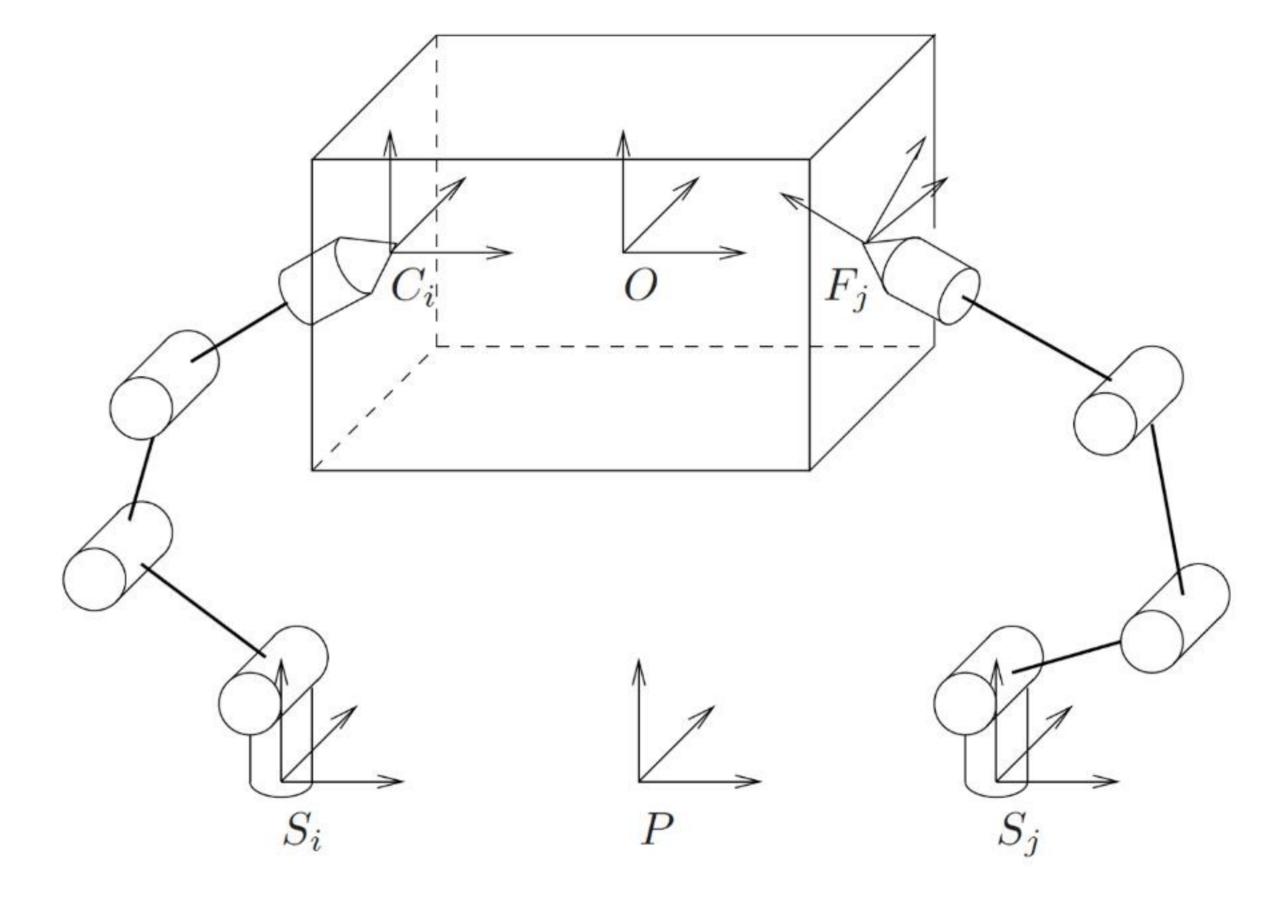


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors
 - These torques will be passed to the tips of the fingers.

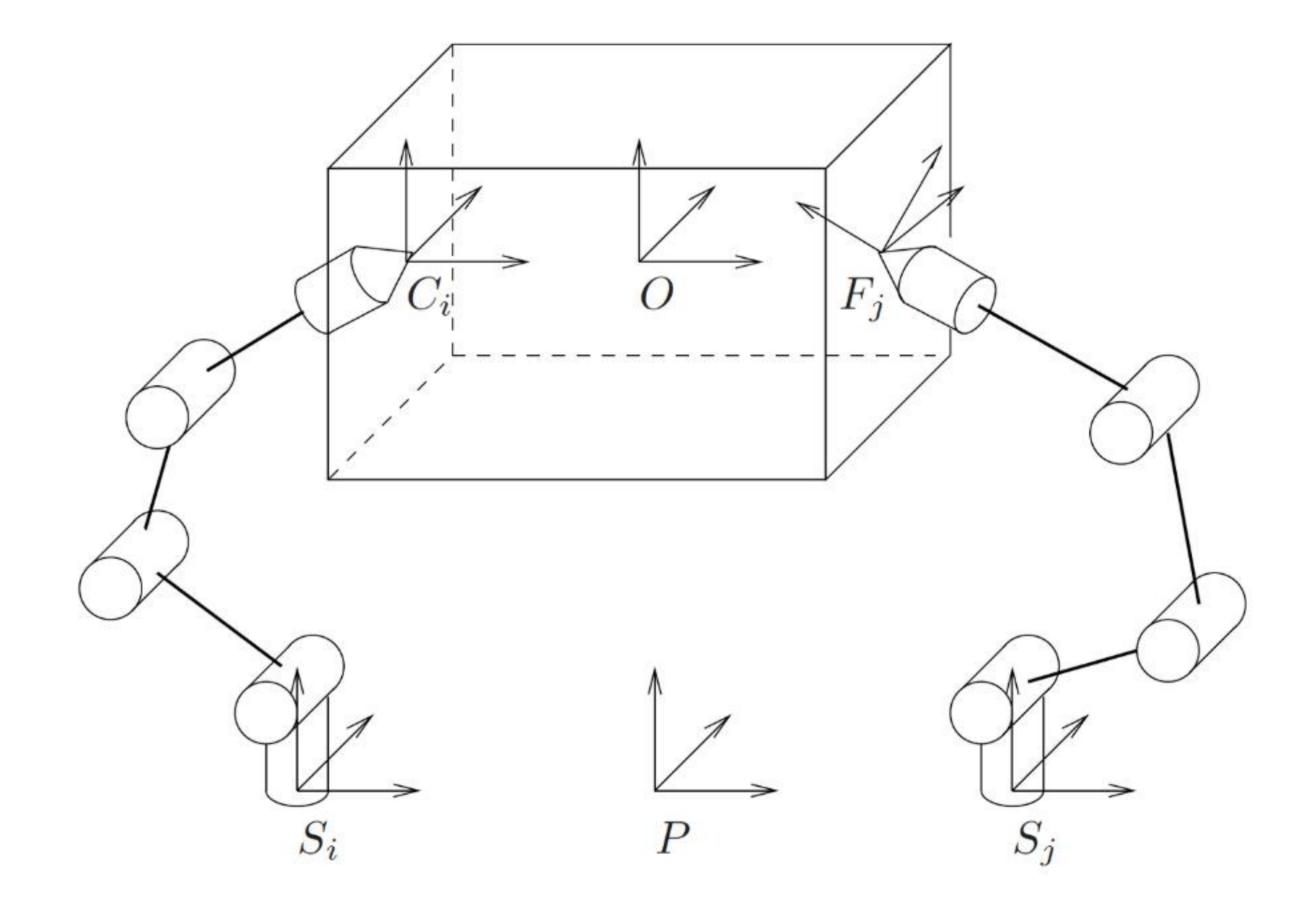


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors
 - These torques will be passed to the tips of the fingers.

0 ...

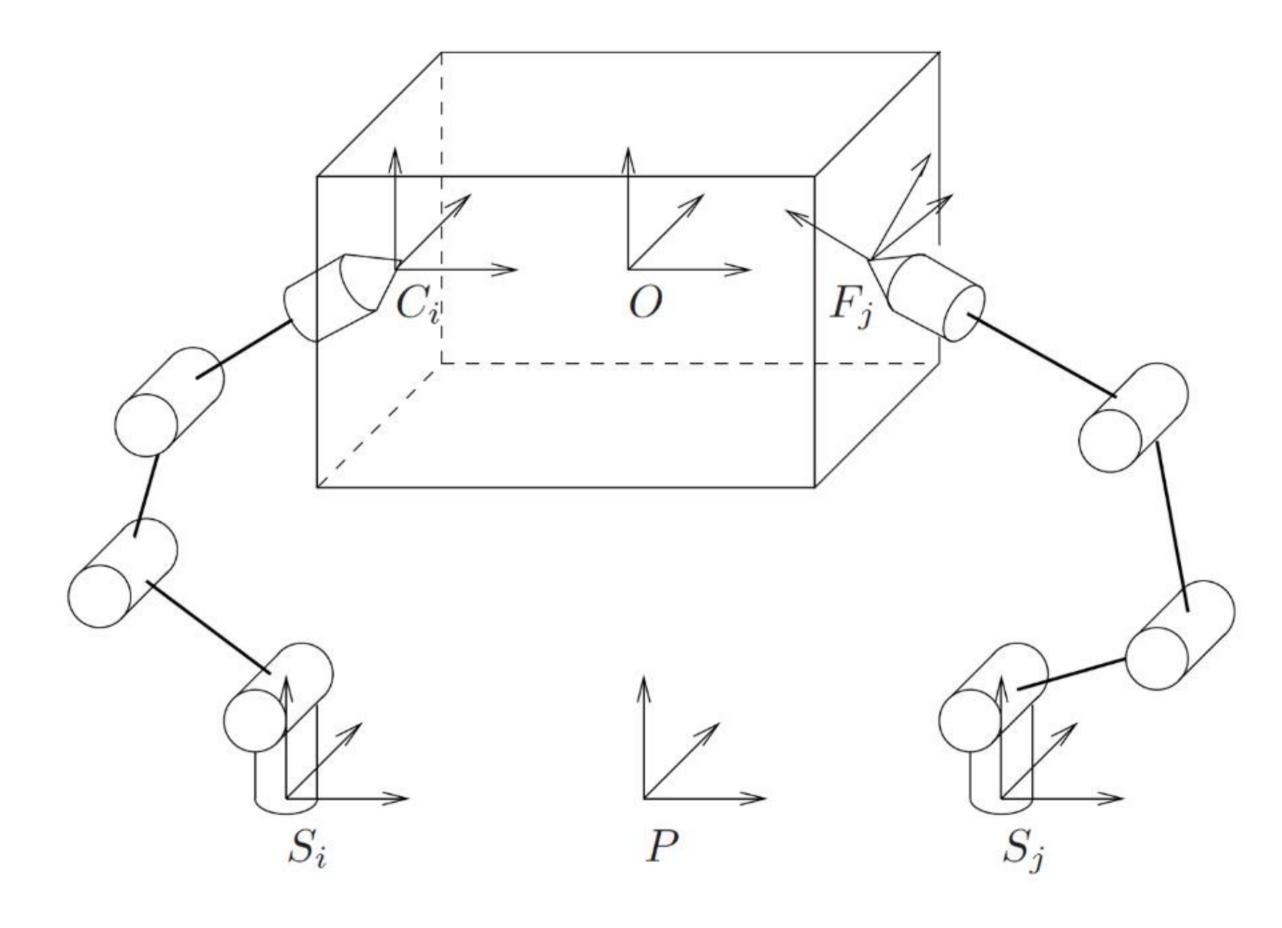


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors
 - These torques will be passed to the tips of the fingers.

0 ...

Q1: How to compute force at the tips from the torques at joints?

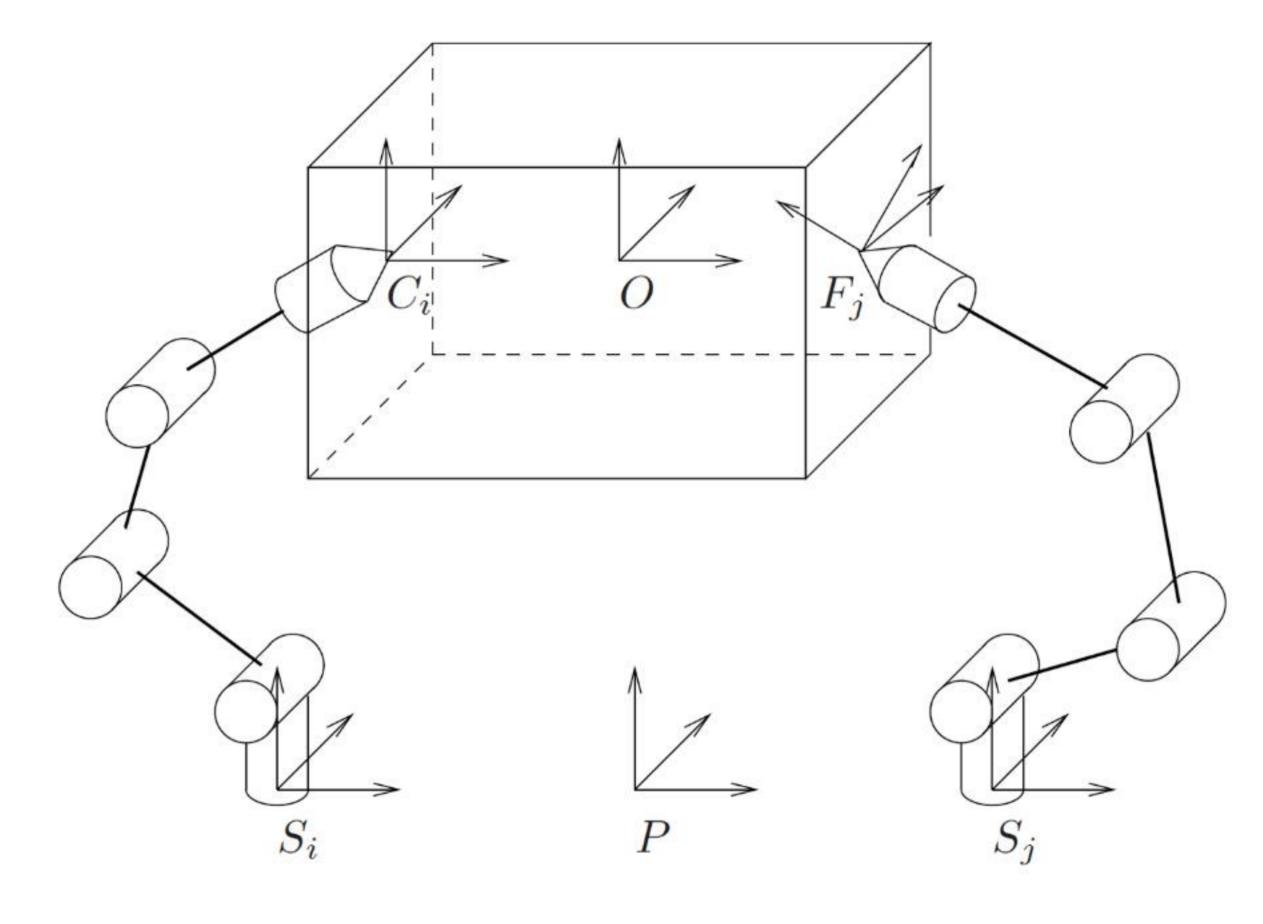


Figure 5.14: Grasp coordinate frames.

- Consider the right grasp problem
 - Assume that we are grasping this box using two arms
 - We apply torques at each joint through the installed motors
 - These torques will be passed to the tips of the fingers.

0 ...

Q1: How to compute force at the tips from the torques at joints?

Q2: To keep the box static, what is the balance condition?

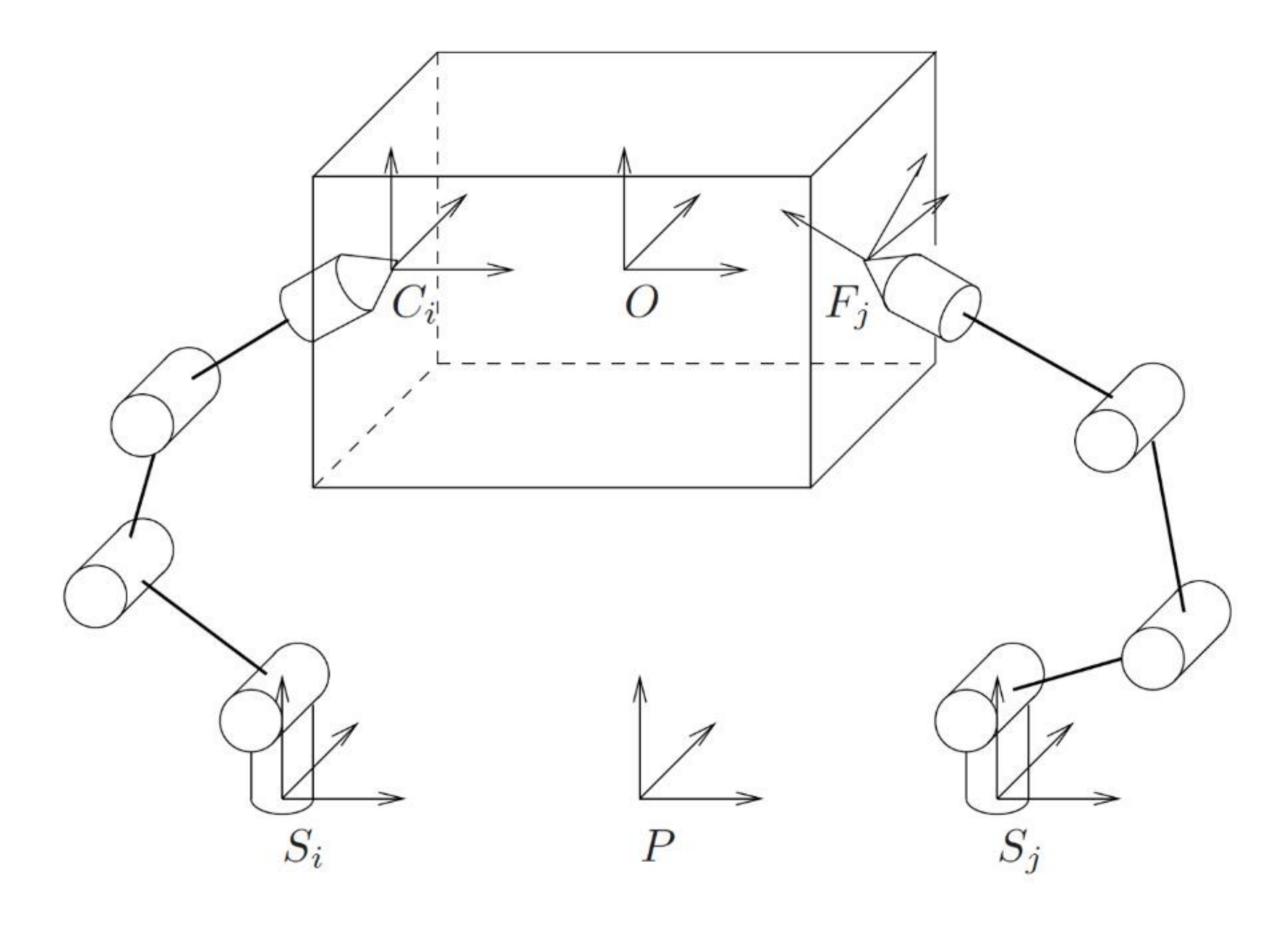


Figure 5.14: Grasp coordinate frames.

- Parameterization
 - $\theta \in \mathbb{R}^n$: vector of joint variables
 - $au \in \mathbb{R}^n$: vector of joint forces/torques

- Parameterization
 - $\theta \in \mathbb{R}^n$: vector of joint variables
 - $\tau \in \mathbb{R}^n$: vector of joint forces/torques
- Task
 - \circ **Forward dynamics:** Determine acceleration $\ddot{ heta}$ given the state $(heta,\dot{ heta})$ and the joint forces/torques

$$\ddot{ heta} = f(au; heta, \dot{ heta})$$

 \circ **Inverse dynamics:** Finding torques/forces given state $heta,\dot{ heta}$ and desired acceleration $\ddot{ heta}$

$$au = g(\ddot{ heta}; heta,\dot{ heta})$$

Lagrangian vs. Newton-Euler Methods

• There are typically two ways to derive the equation of motion for an open-chain robot: Lagrangian method and Newton-Euler method

Lagrangian Formulation

- Energy-based method
- Dynamic equations in closed form
- Often used for study of dynamic properties and analysis of control methods

Newton-Euler Formulation

- Balance of forces/torques
- Dynamic equations numeric/recursive form
- Often used for numerical solution of forward/inverse dynamics

